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A Special Purpose Least Squares Program

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SUMMARY

The relative size, $M(I,J)$, of the seismic signal recorded at station I from the Jth explosion at a particular firing site is assumed to be given by the equation

$$M(I,J) = B(J) + S(I) + \epsilon(I,J),$$

where $B(J)$ depends on the size of the explosion and $S(I)$ is a station term dependent mainly on the distance of the Ith station from the firing site. $M(I,J)$ is measured from seismic records and will usually be in error; $\epsilon(I,J)$ is the error term.

A least squares program is described for estimating: (1) $B(J)$ and $S(I)$, (2) the confidence limits on these quantities, and (3) the differences, and confidence limits on the differences, between all possible pairs of $B(J)$.

Although written for a specific purpose the method is general and can be used to estimate any quantities that can be expressed as equations of the above type.

1. INTRODUCTION

A seismic event radiates elastic waves through the body of the earth. The relative amplitude of these waves as measured at distant recording stations will be determined by two main effects: (1) the size of the event, and (2) the distance of the recording station from the event. The recording instruments and the geology of the recording station and firing site will also have an effect but for explosions from the same firing site these effects will be constant.

If $M(I,J)$ is a measure of the size of the signal (defined as proportional to the log of the measured amplitude) for the Jth explosion at the Ith station, $M(I,J)$ is given by the equation

$$M(I,J) = B(J) + S(I) + \epsilon(I,J), \quad \dots\dots\dots (1)$$

where $B(J)$ depends on the seismic size of the explosion and $S(I)$ is a station term dependent mainly on the distance of the Ith station from the firing site, but including any effects due to recording instruments and geology of the recording station. $M(I,J)$ is measured from seismic records and will usually be in error; $\epsilon(I,J)$ is the error term.

The problem is to estimate (1) $B(J)$ and $S(I)$ (none of which are known), (2) the confidence limits of these quantities, and (3) the differences, and confidence limits on the differences, between the explosion terms. This report describes a computer program for solving this problem by least squares. The program was written by Mr. J. B. Young and is currently in use at Blacknest; it has been given the name LSMF - Least Squares Matrix Factorisation - for historical reasons. The program has developed from others designed to solve the same problem; all these have been titled LSMF. This name has therefore been retained even though "least squares matrix factorisation" is not a very informative title.

2. THE MODEL

Consider t explosions (fired at one test site) and r recording stations. For every station that records one of these explosions there will be an equation of type (1). If all stations record all explosions this results in rt equations. The system is apparently over-determined as there are only $r + t$ unknowns; this however is not so. Each equation only defines $S(I) + B(J)$; there are no equations relating two or more station terms or two or more explosion terms. There is then no unique solution; whatever value is given to one station term, $S(K)$ say, can be allowed for by adjustments to each of the remaining $S(I)$ and $B(J)$ - equation (1) can always be satisfied.

Further assumptions must then be made. The simplest of these is to give one station term a fixed value. As only the relative size of $S(I)$ and $B(J)$ are really important, $M(I,J)$ being a relative value, this would be acceptable except that confidence limits cannot be determined for the $S(I)$ that is assigned the particular value.

To overcome this difficulty equation (1) is rewritten as

$$M(I,J) = B(J) + S(I) + \text{MBAR} + \epsilon(I,J), \quad \dots\dots\dots (2)$$

where MBAR is a constant. As $M(I,J)$ is a purely relative value, the addition of this constant does not materially affect the model. The further assumption is now made that $\sum_j B(J) = 0$ and $\sum_i S(I) = 0$. MBAR can be thought of as the size of the average explosion at the average station; $B(J)$ and $S(I)$ then become corrections to this average for the particular explosion J and station I .

If it is assumed that the errors $\epsilon(I,J)$ are normally distributed with zero mean and variance σ^2 , this model is the same as the widely used analysis of variance model.

3. THE ANALYSIS OF VARIANCE APPROACH

The model described above is simply that of a two way analysis of variance. The data displayed in the usual analysis of variance table are:-

	B(1)	B(2)	...	B(t)
S(1)	M(1,1)	M(1,2)	...	M(1,t)
S(2)	M(2,1)	M(2,2)	...	M(2,t)
S(3)
...
S(r)	M(r,1)	M(r,t)

Now as $\sum I S(I) = 0$ and $\sum J B(J) = 0$ and the expectation of $\epsilon(I, J) = 0$, the average of each column is an estimate of B(J) and the average of each row is an estimate of S(I). The mean value over all M(I, J) gives the value of MBAR. Substituting for S(I), B(J) and MBAR in equation (2) gives the errors $\epsilon(I, J)$; from these errors σ^2 can be estimated and hence the confidence limits obtained.

Unfortunately this method cannot be applied directly because not all M(I, J) are known - stations of low sensitivity fail to record the smaller events and some records are simply not available. The method of least squares however does not require that all M(I, J) be known.

4. THE METHOD OF LEAST SQUARES

Consider the equation

$$y = a_1 x_1 + a_2 x_2 + a_3 x_3 + a_4 x_4 + \dots + a_n x_n, \quad \dots (3)$$

where x_1, \dots, x_n are independent variables; $a_1, a_2, a_3, \dots, a_n$ are unknown coefficients, called the regression coefficients, and y is the dependent variable determined experimentally. Ideally a_1, a_2, \dots, a_n can be found simply by observing n values of y for different values of the independent variables and solving the resulting equations.

Usually, however, the measured value of y will be in error and the problem becomes one of estimating the most probable values of a_1, a_2, \dots, a_n given $m > n$ values of y. This can be done using the principle of least squares which states: if $\epsilon_1, \epsilon_2, \dots, \epsilon_n$ are the errors in m

different equations of type (3) the most probable values of $a_1, a_2, a_3, \dots, a_n$ can be found by making $\epsilon_1^2 + \epsilon_2^2 + \dots + \epsilon_m^2$ (i.e., the sum of the squared errors) a minimum,

$$\text{or } \frac{\partial \sum_i^m \epsilon_i^2}{\partial a_j} = 0 \text{ for } j = 1, n.$$

If $n = 2$ and x_1 is held constant at 1 the problem reduces to the familiar fitting of the "best" straight line.

Suppose that the m equations of type (3) are as follows:-

$$y_1 = a_1 x_{11} + a_2 x_{12} + a_3 x_{13} + \dots + a_n x_{1n} + \epsilon_1$$

$$y_2 = a_1 x_{21} + a_2 x_{22} + a_3 x_{23} + \dots + a_n x_{2n} + \epsilon_2$$

$$\cdot \quad \cdot \quad \cdot \quad \cdot \quad \cdot$$

$$y_m = a_1 x_{m1} + a_2 x_{m2} + a_3 x_{m3} + \dots + a_n x_{mn} + \epsilon_m.$$

These equations are called the equations of condition.

$$\begin{aligned} \text{Now } \sum_i \epsilon_i^2 &= (a_1 x_{11} + a_2 x_{12} + a_3 x_{13} + \dots + a_n x_{1n} - y_1)^2 \\ &+ (a_1 x_{21} + a_2 x_{22} + \dots + a_n x_{2n} - y_2)^2 \\ &+ \dots \\ &+ (a_1 x_{m1} + a_2 x_{m2} + a_3 x_{m3} + \dots + a_n x_{mn} - y_m)^2 \end{aligned}$$

$$\begin{aligned} \text{and } \frac{\partial \sum_i \epsilon_i^2}{\partial a_1} &= 2 \{ (x_{11} x_{11} + x_{21} x_{21} + x_{31} x_{31} + \dots + x_{m1} x_{m1}) a_1 \\ &+ (x_{11} x_{12} + x_{21} x_{22} + \dots + x_{m1} x_{m2}) a_2 \\ &+ (x_{11} x_{1n} + x_{21} x_{2n} + \dots + x_{m1} x_{mn}) a_n \\ &- (x_{11} y_1 + x_{21} y_2 + \dots + x_{m1} y_m) \}. \end{aligned}$$

For the best estimate of $a_1, \frac{\partial \sum_i \epsilon_i^2}{\partial a_1} = 0,$

$$\text{i.e., } a_1 \sum_i (x_{i1})^2 + a_2 \sum_i x_{i1} x_{i2} + \dots + a_n \sum_i x_{i1} x_{in} = \sum_i x_{i1} y_i. \quad \dots (4)$$

The process of deriving equation (4) is equivalent to multiplying each equation of condition by its own coefficient of a_1 ; the coefficient of a_j in equation (4) is then the sum of the coefficients of a_j in these new equations. Similar equations are obtained (equivalent to equating $\frac{\partial \sum \epsilon_i^2}{\partial a_j}$ to zero for $j = 2, n$) by multiplying each equation of condition by its own coefficient of a_j and summing coefficients. This produces n equations, called the normal equations, with n unknowns. In matrix form the normal equations are

$$\begin{bmatrix} \sum x_{i1} x_{i1} & \sum x_{i1} x_{i2} & \cdot & \cdot & \sum x_{i1} x_{in} \\ \sum x_{i2} x_{i1} & \sum x_{i2} x_{i2} & \cdot & \cdot & \sum x_{i2} x_{in} \\ \sum x_{i3} x_{i1} & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot \\ \sum x_{in} x_{i1} & \cdot & \cdot & \cdot & \sum x_{in} x_{in} \end{bmatrix} \begin{bmatrix} a_1 \\ a_2 \\ \cdot \\ \cdot \\ \cdot \\ \cdot \\ a_n \end{bmatrix} = \begin{bmatrix} \sum x_{i1} y_i \\ \sum x_{i2} y_i \\ \cdot \\ \cdot \\ \cdot \\ \cdot \\ \sum x_{in} y_i \end{bmatrix} \dots (5)$$

or $XA = Y$; the X matrix being symmetrical about the diagonal.

The normal equations can usually be solved uniquely. Any of the usual methods can be used, but one method, matrix inversion, has advantages if the confidence limits of the unknowns are required. Matrix inversion is therefore used in the LSMF program.

If the inverse of matrix X is the matrix C

$$\begin{bmatrix} c_{11} & c_{12} & \cdot & \cdot & \cdot & c_{1n} \\ c_{21} & \cdot & \cdot & \cdot & \cdot & \cdot \\ c_{31} & \cdot & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot & \cdot \\ c_{n1} & \cdot & \cdot & \cdot & \cdot & c_{nn} \end{bmatrix}$$

X and C are related by the equation

$$\begin{bmatrix} c_{11} & c_{12} & \dots & c_{1n} \\ c_{21} & \dots & \dots & \dots \\ \dots & \dots & \dots & \dots \\ c_{n1} & \dots & \dots & c_{nn} \end{bmatrix} \begin{bmatrix} \Sigma(x_{i1})^2 & \dots & \Sigma x_{i1}x_{in} \\ \dots & \dots & \dots \\ \dots & \dots & \dots \\ \Sigma x_{in}x_{i1} & \dots & \Sigma x_{in}x_{in} \end{bmatrix} = \begin{bmatrix} 1 & 0 & \dots & 0 \\ 0 & 1 & \dots & 0 \\ \dots & \dots & \dots & \dots \\ 0 & 0 & \dots & 1 \end{bmatrix} \dots (6)$$

The elements of the inverse matrix can be found by expanding to give a series of linear equations.

Thus, the result of multiplying the X matrix by the vth row of the inverse matrix (see also Appendix A) is

$$\begin{aligned}
& c_{v1} \Sigma x_{i1}x_{i1} + c_{v2} \Sigma x_{i1}x_{i2} \dots \dots c_{vn} \Sigma x_{i1}x_{in} = 0 \\
& \dots \\
& c_{v1} \Sigma x_{iv}x_{i1} + c_{v2} \Sigma x_{iv}x_{i2} \dots \dots c_{vn} \Sigma x_{iv}x_{in} = 1 \dots (7) \\
& \dots \\
& \dots
\end{aligned}$$

Solving this set of equations for $c_{v1}, c_{v2}, \dots, c_{vn}$ gives the elements of the vth row of the inverse matrix.

Multiplying equation (5) by C gives

$$A = CY$$

or

$$\begin{bmatrix} a_1 \\ a_2 \\ \dots \\ a_n \end{bmatrix} = \begin{bmatrix} c_{11} & c_{12} & \dots & c_{1n} \\ c_{21} & \dots & \dots & \dots \\ \dots & \dots & \dots & \dots \\ c_{n1} & \dots & \dots & c_{nn} \end{bmatrix} \begin{bmatrix} y_1 \\ y_2 \\ \dots \\ y_n \end{bmatrix} \dots (8)$$

each of the elements of the matrix can then be evaluated as both C and Y are known. The part played by the inverse matrix in determining the confidence limits will be discussed in the next section.

Equation (2) can be put in a form similar to equation (3) as follows:-

$$M(I,J) = 1 \text{ MBAR} + 0 S(1) + \dots + 1 S(I) + \dots + 0 S(r) + \\ 0 B(1) + \dots + 1 B(J) + \dots + 0 B(t) + \epsilon(I,J),$$

$M(I,J)$ is now equivalent to y , the dependent variable, MBAR to a_1 , $S(I)$ and $B(J)$ to the remaining a 's up to a_n and the independent variables are

all either 1 to 0.

To include the assumptions $\sum_I^r S(I) = 0$ and $\sum_J^t B(J) = 0$ two further equations of conditions have to be added:

$$0 = 0 \text{ MBAR} + 1 S(1) + 1 S(2) + \dots + 1 S(I) + \dots + 1 S(r) \\ + 0 B(1) + \dots + 0 B(J) \dots + 0 B(t)$$

and

$$0 = 0 \text{ MBAR} + 0 S(1) + 0 S(2) + \dots + 0 S(J) + \dots + 0 S(r) \\ + 1 B(1) + \dots + 1 B(J) \dots + 1 B(t).$$

Using these equations of condition the normal equations can be derived in exactly the same way as described above.

As an example consider the following set of equations of condition:

$$\begin{bmatrix} 1 & 0 & 0 & 1 & 0 & 0 & 1 \\ 0 & 1 & 0 & 1 & 0 & 0 & 1 \\ 0 & 0 & 1 & 1 & 0 & 0 & 1 \\ 1 & 0 & 0 & 0 & 1 & 0 & 1 \\ 0 & 0 & 1 & 0 & 1 & 0 & 1 \\ 1 & 0 & 0 & 0 & 0 & 1 & 1 \\ 0 & 1 & 0 & 0 & 0 & 1 & 1 \\ 0 & 0 & 1 & 0 & 0 & 1 & 1 \\ 0 & 0 & 0 & 1 & 1 & 1 & 0 \\ 1 & 1 & 1 & 0 & 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} S(1) \\ S(2) \\ S(3) \\ B(1) \\ B(2) \\ B(3) \\ \text{MBAR} \end{bmatrix} = \begin{bmatrix} 2.0 \\ 3.0 \\ 4.0 \\ 4.0 \\ 4.0 \\ 4.0 \\ 5.0 \\ 7.0 \\ 0.0 \\ 0.0 \end{bmatrix}$$

In this example it is assumed that station S(2) did not record explosion B(2).

Multiplying each equation of condition by its own coefficient of S(1) and summing coefficients gives the first normal equation

$$4 S(1) + S(2) + 1 S(3) + 1 B(1) + 1 B(2) + 1 B(3) + 3 \text{ MBAR} = 10.0.$$

Multiplying each equation of condition by its own coefficient of S(2) and summing gives

$$1 S(1) + 3 S(2) + 1 S(3) + 1 B(1) + 0 B(2) + 1 B(3) + 2 \text{ MBAR} = 8.00.$$

Similar normal equations can be obtained for S(3), B(1), B(2), B(3) and MBAR.

In matrix form the equations are

$$\begin{bmatrix}
 4 & 1 & 1 & . & 1 & 1 & 1 & . & 3 \\
 & & . & & & & & & . \\
 1 & 3 & 1 & . & 1 & 0 & 1 & . & 2 \\
 & & . & & & & & & . \\
 1 & 1 & 4 & . & 1 & 1 & 1 & . & 3 \\
 - & - & - & - & - & - & - & - & - \\
 & & . & & & & & & . \\
 1 & 1 & 1 & . & 4 & 1 & 1 & . & 3 \\
 & & . & & & & & & . \\
 1 & 0 & 1 & . & 1 & 3 & 1 & . & 2 \\
 & & . & & & & & & . \\
 1 & 1 & 1 & . & 1 & 1 & 4 & . & 3 \\
 - & - & - & - & - & - & - & - & - \\
 3 & 2 & 3 & & 3 & 2 & 3 & . & 8
 \end{bmatrix}
 \begin{bmatrix}
 S(1) \\
 S(2) \\
 S(3) \\
 \\
 B(1) \\
 B(2) \\
 B(3) \\
 \\
 \text{MBAR}
 \end{bmatrix}
 =
 \begin{bmatrix}
 10.0 \\
 \\
 8.0 \\
 \\
 15.0 \\
 \\
 \\
 \\
 9.0 \\
 8.0 \\
 16.0 \\
 \\
 33.0
 \end{bmatrix}
 \dots (9)$$

A series of linear equations has a unique solution if the determinant of the coefficients of the unknowns is not zero. The determinant of the matrix of coefficients in equation (9) is non-zero, but if equation (1) is

used as the model it can easily be shown that the determinant of coefficients is zero. Thus, the normal equations now become

$$\begin{bmatrix} 3 & 0 & 0 & 1 & 1 & 1 \\ 0 & 2 & 0 & 1 & 0 & 1 \\ 0 & 0 & 3 & 1 & 1 & 1 \\ 1 & 1 & 1 & 3 & 0 & 0 \\ 1 & 0 & 1 & 0 & 2 & 0 \\ 1 & 1 & 1 & 0 & 0 & 3 \end{bmatrix} \begin{bmatrix} S(1) \\ S(2) \\ S(3) \\ B(1) \\ B(2) \\ B(3) \end{bmatrix} = \begin{bmatrix} 10.0 \\ 8.0 \\ 15.0 \\ 9.0 \\ 8.0 \\ 16.0 \end{bmatrix}$$

Adding row 2 and 3 to row 1 and rows 5 and 6 to row 4 makes the new rows 1 and 4 identical. Subtracting row 4 from row 1 makes all row 1 zero; hence the determinant is zero. This is true of any matrix based on equation (1).

5. CONFIDENCE LIMITS

Estimates of the regression coefficients can be found by solving the normal equations. As a measure of the reliability of these estimates it is useful to compute the limits, called confidence limits, of the range within which the true value of the regression coefficients can be expected to lie with a given probability. The smaller this range turns out to be the more reliable are the estimates.

Consider the simple case of a random variable normally distributed with variance σ^2 and mean ξ , then it is easily shown that any item picked at random from such a population will lie between $\xi + 1.96\sigma$ and $\xi - 1.96\sigma$ (or in words within roughly two standard deviations of the mean) with a 95% probability, i.e., 19 times in 20.

Confidence limits are arrived at in a similar way; the main difference is that ξ and σ are not known and have to be estimated.

The estimates of the regression coefficients are analogous to the mean in the above simple example. To estimate the variance requires a more detailed study of equation (8). Expanding equation (8)

$$\begin{aligned}
a_1 &= c_{11} \sum_i^m x_{i1} y_i + c_{12} \sum_i^m x_{i2} y_i \cdot \cdot \cdot + c_{1n} \sum_i^m x_{in} y_i \\
a_2 &= c_{21} \sum_i^m x_{i1} y_i + c_{22} \sum_i^m x_{i2} y_i \cdot \cdot \cdot + c_{2n} \sum_i^m x_{in} y_i \\
&\cdot \quad \cdot \quad \cdot \quad \cdot \\
&\cdot \quad \cdot \quad \cdot \quad \cdot \\
a_v &= c_{v1} \sum_i^m x_{i1} y_i + c_{v2} \sum_i^m x_{i2} y_i \cdot \cdot \cdot + c_{vn} \sum_i^m x_{in} y_i \quad \dots (10) \\
&\cdot \quad \cdot \quad \cdot \quad \cdot \\
&\cdot \quad \cdot \quad \cdot \quad \cdot \\
&\cdot \quad \cdot \quad \cdot \quad \cdot
\end{aligned}$$

Rearranging (10)

$$a_v = \sum_i^m y_i [c_{v1} x_{i1} + c_{v2} x_{i2} + \cdot \cdot \cdot + c_{vn} x_{in}], \quad \dots (11)$$

which shows that a_v is a linear function of y_i .

Now the quantity in square brackets in equation (11) is solely a function of the independent variables and can be represented by a single quantity, say k_{vi} .

Then

$$a_v = \sum_i^m y_i k_{vi}$$

and (using equation (B3), Appendix B)

$$V [a_v] = \sum_i^m k_{vi}^2 V[y_i] = \sigma^2 \sum_i^m k_{vi}^2,$$

where $V[a_v]$ is understood to mean the variance of a_v and σ^2 is the variance of y_i , i.e., the variance of the errors ϵ_i . It can also be shown that, because a_v is a linear function of y_i which is normally distributed, a_v will also be normally distributed [1].

Now σ^2 is not known, so $V[a_v]$ cannot be determined. An estimate of σ^2 , s^2 say, can however be obtained. Thus,

$$s^2 = \frac{\sum (\epsilon_i')^2}{m - n},$$

where m is the number of equations of condition and n is the number of

1. K. A. Brownlee: (1965) "Statistical Theory and Methodology in Science and Engineering". John Wiley and Sons Incorporated, New York.

unknowns (regression coefficients). The quantity $m - n$ is called the number of degrees of freedom. An estimate of the errors ϵ'_i is obtained by substituting the regression coefficients in the equations of condition.

As a_v is normally distributed with variance $s^2 \sum_{i=1}^m k_{vi}^2$, the 95% confidence limits should then be $a_v \pm 1.96 \sqrt{s^2 \sum_{i=1}^m k_{vi}^2}$. This is only true if the degrees of freedom D is very large. For small D , s^2 is a less reliable estimate of σ^2 ; to allow for this the confidence limits become $a_v \pm t \sqrt{s^2 \sum_{i=1}^m k_{vi}^2}$, where t (called Students t) depends on the degrees of freedom and is > 1.96 . (Tables of Students t for various degrees of freedom and level of probability are given in most books on statistics.)

To determine the confidence limits $\sum_{i=1}^m k_{vi}^2$ must be evaluated. At first sight this appears a formidable task; it can however be shown that $\sum_{i=1}^m k_{vi}^2$ is simply c_{vv} ; the v th diagonal element in the inverted matrix.

This can be demonstrated as follows:-

$$\begin{aligned} \sum_{i=1}^m k_{vi}^2 &= \sum_{i=1}^m k_{vi} k_{vi} \\ &= \sum_{i=1}^m k_{vi} [c_{v1} x_{i1} + c_{v2} x_{i2} + \dots + c_{vn} x_{in}] \\ &= c_{v1} \sum_{i=1}^m k_{vi} x_{i1} + c_{v2} \sum_{i=1}^m k_{vi} x_{i2} + \dots + c_{vn} \sum_{i=1}^m k_{vi} x_{in} \end{aligned}$$

Considering now only the c_{vh} term of the right hand side,

$$\begin{aligned} c_{vh} \sum_{i=1}^m k_{vi} x_{ih} &= c_{vh} \sum_{i=1}^m [c_{v1} x_{i1} + \dots + c_{vn} x_{in}] x_{ih} \\ &= c_{vh} [c_{v1} \sum_{i=1}^m x_{i1} x_{ih} + c_{v2} \sum_{i=1}^m x_{i2} x_{ih} + \dots \\ &\quad \dots + c_{vn} \sum_{i=1}^m x_{in} x_{ih}]. \end{aligned}$$

When $h = v$ the quantity in the square brackets is identical to the left hand side of an equation formed by multiplying the v th row of the C matrix by the v th column of the X matrix; from (6) this is equal to 1. For $h \neq v$ the quantity in square brackets is identical to the left hand side of one of the other equations (6); the right hand side of all these equations is zero.

Thus, $\sum_{i=1}^m k_{vi}^2 = c_{vv}$, the v th diagonal element of the inverted matrix.

and $V[a_v] = c_{vv} s^2$; it is because of this that matrix inversion is used for solving the normal equations.

To get the confidence limits on the difference of two a's, a_v and a'_v the variance on the difference is required, i.e., $V[a_v - a'_v]$. Now $V[a_v - a'_v] = V[a_v] + V[a'_v] - 2 \text{Cov}[a_v, a'_v]$, where $\text{Cov}[a_v, a'_v]$ is the covariance of a_v, a'_v (for proof see Appendix B). By an analysis similar to that given for $V[a_v]$ it can be shown that

$$\text{Cov}[a_v, a'_v] = s^2 c'_{vv},$$

i.e., the product of the variance of the errors and the element of the inverse matrix that lies at the intersection of the vth row and the vth column (or vice versa - the two elements c_{vv} , and c'_{vv} are equal because the inverse matrix is also symmetrical).

The variance of the differences of two a's is then given by

$$V[a_v - a'_v] = s^2(c_{vv} + c'_{vv} - 2 c_{vv}).$$

The 95% confidence limits of $a_v - a'_v$ is then $t\sqrt{V[a_v - a'_v]}$.

Confidence limits on MBAR, S(I), B(J) and on the differences between each pair of explosion terms (B(J's)), are calculated by the methods outlined above. As the M(I,J)'s are only relative values the confidence limits on the absolute values of MBAR, S(I) and B(J) have little meaning. The confidence limits on the differences of the explosion terms are however valuable as they are confidence limits on the absolute differences between the seismic sizes of pairs of explosions.

6. WEIGHTING

So far it has been assumed that the errors in the dependent variables all have the same variance σ^2 . This may not be so; some measurements may be known with greater (absolute) accuracy. To get the best estimate of the regression coefficients, i.e. the one with minimum variance, each equation of condition should be weighted by a factor \sqrt{w} , where $w = \frac{1}{\sigma_i^2}$; σ_i^2 is the variance of the ith measurement (for a discussion of weighting see reference [1]). A facility for weighting any equation of condition has therefore been included in the LSMF program, although σ_i^2 will usually be difficult to estimate.

7. THE PROGRAM

The program will accept data for up to 60 explosions recorded at a maximum of 200 stations. The input to the program is:-

- (1) Students t tables for the 95% probability level.
- (2) A title for the data being processed and any number of comment cards.

1. E. Whittaker and G. Robinson: (1944) "The Calculus of Observations: A Treatise on Numerical Mathematics". Fourth Edition, Blackie, London and Glasgow

- (3) An identification code for each station.
- (4) An identification code for each explosion.
- (5) Cards with station code, event code, $M(I,J)$ and the weight to be assigned to $M(I,J)$. If the weight is left blank it is taken to be unity.

The matrix of coefficients of the normal equations (the X matrix) are then set up. This could be done as outlined in Section 4, i.e., by setting up all the equations of condition then multiplying each equation by the coefficient of each unknown in turn and summing. This would need a large amount of storage space in the machine to little purpose as most of the terms in the equations of condition are zero (cf, the example given in Section 4). A method of constructing the matrix of coefficients directly has therefore been devised. As a result of this a far larger number of unknowns (260) can be handled by the program than would be possible if the equations of condition had to be stored in their entirety.

The X matrix is set up as follows: first the whole matrix is zeroed. Each non-zero element of the X matrix is now computed from the input data and stored in its appropriate place in the matrix. As the resultant matrix is symmetrical about the diagonal only the upper triangular matrix and the diagonal elements have to be computed. The upper triangular elements, X_{ij} , are then repeated in the lower triangular position X_{ji} . For the purposes of construction the matrix can be divided into 7 parts (see Figure 1). The equivalent 7 parts are shown in dotted outline in equation (9)).

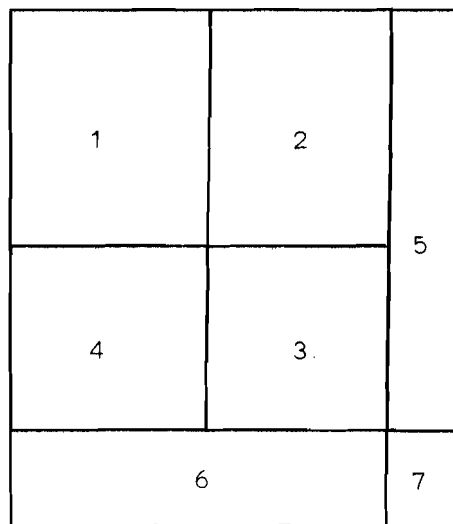


FIGURE 1

If t is the number of explosions read in and r the number of stations, part 1 is an $r \times r$ matrix, part 3 a $t \times t$ matrix, parts 2 and 4 are $r \times t$ matrices, part 2 having t columns and r rows and part 4, r columns and t rows, parts 5 and 6 are $(r + t) \times 1$ matrices and part 7 is a single element.

Matrix 2 is constructed first. The first element in the first row of this matrix is unity if S(1) is recorded at station B(1), the second element is unity if S(1) recorded B(2) and so on to B(t). Similarly in the second row the first element is unity if S(2) recorded B(1), the second element if S(2) recorded B(2) and so on. Rows 3, 4, t of matrix 2 are constructed in a similar way. Matrix 4 is now constructed by reflecting matrix 2 in the diagonal.

The diagonal elements of matrix 1 are now formed by summing the corresponding row of matrix 2 and the diagonal elements of matrix 3 by summing the corresponding rows of matrix 4. The diagonal elements of 1 and 3 are now repeated in order in the column matrix 5 and the row matrix 6. Element 7 is half the sum of the elements in the column matrix 5. Finally 1 is added to each element of matrices 1 and 3.

The above somewhat involved process produces the correct matrix of normal equations with $(r + t + 1)^2$ elements.

The first element of the right hand side of equation (5) is formed by summing all $M(1,J)$ (it is assumed that $M(I,J) = 0$ if station I did not record explosion J), the second element by summing all $M(2,J)$ and so on. Element r of the right hand side is then $\sum_J M(r,J)$. Element r + 1 is $\sum_I M(I,1)$ element r + 2 is $\sum_I M(I,2)$ and so on. Element r + t + 1 is $\sum_{IJ} M(I,J)$.

The setting up of the normal equations has been described assuming all the data were to be given equal weight. If the weights are not unity (but w) the elements of parts 2 and 4 of the matrix are now replaced by the weights, w, and the setting up of the matrix then proceeds as before.

To take account of weighting when setting up the right hand side of equation (5) each $M(I,J)$ is multiplied by its weight and then summed as before.

The matrix of the coefficients of the normal equations is now inverted using a subroutine from the Harwell Program Library (No. MB01A). This subroutine uses the so called triangular decomposition method of matrix inversion [1].

Both the original matrix and the inverted matrix are stored on disk.

Using the inverted matrix S(I), B(J) and MBAR are computed. Subtracting these values from the original $M(I,J)$ gives the error term $\epsilon(I,J)$ and hence s^2 the estimate of the variance of the errors can be found. From s^2 and the elements of the inverted matrix the

1. HMSO: (1961) "Modern Computing Methods". National Physical Laboratory. HMSO, London

confidence limits on $S(I)$, $B(J)$ and $MBAR$ and on the differences between pairs of $B(J)$ are computed.

The output from the program is:-

- (1) Tables showing stations and events used and input data, $M(I,J)$, with weights.
- (2) Tables showing the residuals $\epsilon(I,J)$.
- (3) Tables showing best estimates of $S(I)$, $B(J)$ and $MBAR$ their variances and 95% confidence limits.
- (4) Tables showing differences between each pair of $B(J)$ and the 95% confidence limits of these differences.
- (5) Table showing variables used in the calculations.

Although the program described here has been written to solve a particular problem the program could equally well be used for any problem that can be expressed in terms of the model given in Section 2; this is the familiar two way analysis of variance model.

To carry out a two way analysis of variance using the usual techniques the values of all the elements in the analysis of variance table must be known (one or two missing values can be tolerated). No such restriction applies to this program.

APPENDIX A

MATRICES AND MATRIX INVERSION

A matrix is an array of numbers of the form

$$\begin{bmatrix} a_{11} & a_{12} & \cdot & \cdot & \cdot & a_{1j} & \cdot & \cdot & \cdot & a_{1n} \\ a_{21} & a_{22} & & & & \cdot & & & & \cdot \\ \cdot & \cdot & & & & \cdot & & & & \cdot \\ \cdot & \cdot & & & & \cdot & & & & \cdot \\ a_{i1} & a_{i2} & \cdot & \cdot & \cdot & a_{ij} & \cdot & \cdot & \cdot & a_{in} \\ \cdot & \cdot & & & & \cdot & & & & \cdot \\ \cdot & \cdot & & & & \cdot & & & & \cdot \\ a_{m1} & a_{m2} & \cdot & \cdot & \cdot & a_{mj} & \cdot & \cdot & \cdot & a_{mn} \end{bmatrix}$$

Unlike determinants, matrices cannot be evaluated to give a single value. They can however be represented by a single quantity, say A , and as such used in many algebraic operations just as if A were a single number.

For example the addition of the matrices A and B means summing corresponding elements of the two matrices. Thus if

$$\begin{aligned} A &= \begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix} \\ \text{and} \quad B &= \begin{bmatrix} b_{11} & b_{12} \\ b_{21} & b_{22} \end{bmatrix} \\ A + B &= \begin{bmatrix} a_{11} + b_{11}, & a_{12} + b_{12} \\ a_{21} + b_{21}, & a_{22} + b_{22} \end{bmatrix} \end{aligned}$$

Multiplication of two matrices is more complicated. Thus,

$$AB = \begin{bmatrix} a_{11}b_{11} + a_{12}b_{21}, & a_{11}b_{12} + a_{12}b_{22} \\ a_{21}b_{11} + a_{22}b_{21}, & a_{21}b_{12} + a_{22}b_{22} \end{bmatrix}$$

Each element of the new matrix is formed by multiplying each element in a row of the first matrix by the corresponding element in the column of the second matrix and summing. For multiplication to be possible the second matrix (matrix B) must have the same number of rows as the first matrix has columns.

Matrices find their widest application in the solution of linear equations.

Consider the equations

$$\begin{aligned}
 a_{11}x_1 + a_{12}x_2 + a_{13}x_3 + \dots + a_{1n}x_n &= y_1 \\
 a_{21}x_1 + a_{22}x_2 + a_{23}x_3 + \dots + a_{2n}x_n &= y_2 \\
 &\dots \dots \dots (A1) \\
 &\dots \dots \dots \\
 a_{n1}x_1 + a_{n2}x_2 + a_{n3}x_3 + \dots + a_{nn}x_n &= y_n
 \end{aligned}$$

These equations can be represented in matrix form as

$$\begin{bmatrix} a_{11} & a_{12} & \dots & a_{1j} & \dots & a_{1n} \\ a_{21} & a_{22} & \dots & \dots & \dots & \dots \\ \dots & \dots & \dots & \dots & \dots & \dots \\ \dots & \dots & \dots & \dots & \dots & \dots \\ a_{i1} & a_{i2} & \dots & a_{ij} & \dots & a_{in} \\ \dots & \dots & \dots & \dots & \dots & \dots \\ a_{n1} & \dots & \dots & a_{nj} & \dots & a_{nn} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ \dots \\ \dots \\ \dots \\ \dots \\ a_n \end{bmatrix} = \begin{bmatrix} y_1 \\ y_2 \\ \dots \\ \dots \\ \dots \\ \dots \\ y_n \end{bmatrix} \dots \dots (A2)$$

$Ax = y.$

Strictly the term matrix is applied only to A; the column matrices x and y are called vectors.

The solution of (A2) can be represented symbolically as

$$x = A^{-1}y, \dots \dots (A3)$$

where A^{-1} is called the inverse matrix of A.

Now just as in ordinary algebra

$$aa^{-1} = 1,$$

so a unit matrix I can be defined such that

$$AA^{-1} = I, \dots \dots (A4)$$

where

$$I = \begin{bmatrix} 1 & 0 & 0 & \dots & 0 \\ 0 & 1 & 0 & \dots & 0 \\ 0 & \dots & 1 & \dots & \dots \\ \dots & \dots & \dots & \dots & \dots \\ 0 & 0 & 0 & \dots & 1 \end{bmatrix}$$

all the elements of I are zero except the diagonal elements which are unity. Operating on a matrix with I leaves the matrix unchanged, i.e., $AI = A$.

Equation (A4) provides a way of determining A^{-1} . Let c_{ij} be the element of the inverse matrix; then writing out (A4) in full

$$\begin{bmatrix} a_{11} & a_{12} & \dots & a_{1n} \\ a_{21} & a_{22} & \dots & a_{2n} \\ \dots & \dots & \dots & \dots \\ a_{n1} & a_{n2} & \dots & a_{nn} \end{bmatrix} \begin{bmatrix} c_{11} & c_{12} & \dots & c_{1n} \\ c_{21} & c_{22} & \dots & c_{2n} \\ \dots & \dots & \dots & \dots \\ c_{n1} & c_{n2} & \dots & c_{nn} \end{bmatrix} = \begin{bmatrix} 1 & 0 & 0 & 0 & \dots & 0 \\ 0 & 1 & 0 & 0 & \dots & 0 \\ 0 & 0 & 1 & \dots & \dots & \dots \\ \dots & \dots & \dots & \dots & \dots & \dots \\ 0 & \dots & \dots & \dots & \dots & 1 \end{bmatrix}$$

Carrying out the multiplication of the left hand side. The result of multiplying the a_{ij} matrix by the first column of the C matrix is

$$\begin{aligned} a_{11}c_{11} + a_{12}c_{21} + \dots + a_{1n}c_{n1} &= 1 \\ a_{21}c_{11} + a_{22}c_{21} + \dots + a_{2n}c_{n1} &= 0 \\ \dots & \dots \\ a_{n1}c_{11} + a_{n2}c_{21} + \dots + a_{nn}c_{n1} &= 0. \end{aligned}$$

This group of n equations has n unknowns $c_{11}, c_{21}, c_{31}, \dots, c_{n1}$: the elements of the first column of the C matrix, $c_{11}, c_{21}, \dots, c_{n1}$ can therefore be obtained by solving this set of equations.

A similar group of equations can be obtained by multiplying the A matrix and the second column of the C matrix. The elements in each column of the C matrix can therefore be evaluated in turn; this results in the inverse matrix.

The right hand side of equation (A2) can then be operated on with the inverse matrix to give x as shown in equation (A3).

Writing out (A3) in full

$$\begin{bmatrix} x_1 \\ x_2 \\ \cdot \\ \cdot \\ \cdot \\ x_n \end{bmatrix} = \begin{bmatrix} c_{11} & c_{12} & \cdot & \cdot & \cdot & c_{1n} \\ c_{21} & c_{22} & \cdot & \cdot & \cdot & c_{2n} \\ \cdot & \cdot & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot & \cdot & \cdot \\ c_{n1} & c_{n2} & \cdot & \cdot & \cdot & c_{nn} \end{bmatrix} \begin{bmatrix} y_1 \\ y_2 \\ \cdot \\ \cdot \\ \cdot \\ y_n \end{bmatrix}$$

i.e.,

$$x_1 = c_{11}y_1 + c_{12}y_2 + c_{13}y_3 + \cdot + \cdot + c_{1n}y_n \quad \dots (A5)$$

$$x_2 = c_{21}y_1 + c_{22}y_2 + c_{23}y_3 + \cdot + \cdot + c_{2n}y_n$$

$$\cdot \quad \cdot \quad \cdot \quad \cdot \quad \cdot \quad \cdot$$

$$\cdot \quad \cdot \quad \cdot \quad \cdot \quad \cdot \quad \cdot$$

As the c's are known and the y's are known the equations (A5) give x_1, x_2, \dots, x_n the solutions of (A1).

Shorter methods of solving linear equations are available, e.g., Gaussian elimination but matrix inversion has advantages if several sets of equations have to be solved with the same left hand side but different right hand side. Once the inverse of a particular left hand side has been computed it can be used to solve any number of sets of equations simply by operating on the y matrices. Another advantage of the inverse matrix is that it allows the confidence limits of the unknowns to be computed easily in least squares problems (see Section 5).

APPENDIX B

SOME STATISTICAL CONCEPTS AND PROOFS

B1. EXPECTATION

The expectation of a random variable x , usually written $E[X]$, is defined as

$$E[X] = \int_{-\infty}^{\infty} xp(x)dx,$$

where $p(x)$ is the probability that the random variable will take the particular value x . The expectation corresponds to the mean of the whole population of x . Means determined from a set of sample values of x will not usually coincide with $E[X]$ but will approach $E[X]$ as the sample size increases.

The expectation of a constant is the constant, since the constant can take only one value. The expectation of an expected value, $E[E[X]]$, is simply $E[X]$ since $E[X]$ is a constant and as shown above this only has one value.

B2. VARIANCE

Variance measures the spread of a distribution and can be defined on terms of expectation thus,

$$V[X] = E[(X - E[X])^2], \quad \dots\dots (B1)$$

or in words the variance is the expected value (average value) of the squared deviation of a random variable from its expectation.

An alternative form of (B1) is

$$V[X] = E[X^2] - (E[X])^2. \quad \dots\dots (B2)$$

If a and b are constants the variance of a linear function of X , say $a + bX$, is

$$\begin{aligned} V[a + bX] &= E[((a + bX) - (E[a + bX]))^2] \\ &= E[a^2] + 2abE[X] + b^2E[X^2] - a^2 - 2abE[X] \\ &\quad - b^2(E[X])^2 \\ &= b^2\{E[X^2] - (E[X])^2\} \\ &= b^2V[X]. \end{aligned}$$

If Z is the difference of two random variables X and Y , i.e., $Z = X - Y$

$$\begin{aligned}
 V[Z] &= E[Z^2] - (E[Z])^2 \text{ using (B2)} \\
 &= E[(X - Y)^2] - (E[X - Y])^2 \\
 &= E[(X^2 - XY + Y^2)] - (E[X])^2 + 2E[X]E[Y] \\
 &\quad - (E[Y])^2 \\
 &= E[X^2] - (E[X])^2 + E[Y^2] - (E[Y])^2 \\
 &\quad - 2(E[XY] - E[X]E[Y]) \\
 &= V[X] + V[Y] - 2 \text{Cov}[X, Y].
 \end{aligned}$$

$\text{Cov}[X, Y]$ is called the covariance of X and Y and is defined as $E[XY] - E[X]E[Y]$.

The results given above can be generalised for any linear combination of random variables. Thus, if

$$\begin{aligned}
 Z &= a_0 + a_1 X_1 + \dots + a_n X_n \\
 V(Z) &= \sum_i^n a_i^2 V[X_i] + \sum_{i \neq j}^{nn} a_i a_j \text{Cov}[X_i, X_j] \\
 &\quad i \neq j.
 \end{aligned}$$

If the random variables are uncorrelated their covariances are zero. If also $V[X_i]$ is constant and equal to σ^2 for all i then

$$V(Z) = \sigma^2 \sum_i^n a_i^2. \quad \dots (B3)$$

KEMPTHORNE O. THE DESIGN AND ANALYSIS OF EXPERIMENTS. BOTH BOOKS ARE PUBLISHED IN THE WILEY SERIES IN STATISTICS.

NON-STANDARD LIBRARY SUBPROGRAMS USED

EDUMP DUMP ROUTINE
SDATE DATE IN ALPHANUMERIC FORM DD/MM/YY
SECCLK PICKS UP SECONDS CLOCK READING
EXIT ROUTINE TO BRANCH BACK TO MACHINE CONTROL

VARIABLES USED

A IS THE MATRIX
B IS THE SUM OF MEASURED MAGNITUDES
C IS THE DIAGONAL OF THE INVERTED MATRIX
X ARRAY CONTAINS STATION (FOLLOWED BY EVENT) CORRECTIONS
Y ARRAY CONTAINS EVENT CORRECTIONS
CLX CONFIDENCE LIMITS OF X
CLY CONFIDENCE LIMITS OF Y
VARX VARIANCE OF X
VARY VARIANCE OF Y

NST = TOTAL NUMBER OF STATIONS
NBT = TOTAL NUMBER OF EVENTS
NR = TOTAL NUMBER OF READINGS
NRS = NUMBER OF EVENTS PER STATION
NRB = NUMBER OF STATIONS PER EVENT
NS = STATION COUNT
NB = EVENT COUNT
J = COLUMN COUNT
I = ROW COUNT
N = SIZE OF MATRIX

MAXIMUM NUMBER OF STATIONS = 200
MAXIMUM NUMBER OF EVENTS = 60

THE DATA DECK SHOULD BE MADE UP AS FOLLOWS --

- 1) HEADING CARD WHICH WILL BE REPRINTED AT THE TOP OF EACH PAGE
PUNCH THE FIRST 72 COLUMNS ONLY COLS.73-80 FOR CONTINUATION COUNT
FOLLOWED BY ANY NUMBER OF COMMENT CARDS
TILL A ZERO IS ENCOUNTERED IN THE LAST COLUMN
 - 2) STATIONS IN ORDER REQUIRED IN MATRIX
STATION CARDS ARE READY-PUNCHED
FOLLOWED BY END STATIONS CARD
 - 3) EVENT CODES IN ORDER REQUIRED IN MATRIX
EVENT CODE (8 CHARS.) - START PUNCHING IN COLUMN 7
EVENT DATA AND COMMENTS - START PUNCHING IN COLUMN 20
FOLLOWED BY END EVENTS CARD
 - 4) MAGNITUDE DATA
STATION CODE COLUMNS 2-6
EVENT CODE COLUMNS 7-14
MAGNITUDE DECIMAL POINT (.) IN COLUMN 20 (3 DP)
WEIGHTING FACTOR IN COLUMN 30
IF WEIGHTING FACTOR ZERO ASSUMED TO BE 1
FOLLOWED BY END MAGNITUDES CARD
- OPTION IF THIS LAST CARD IS BLANK NO COMPUTATION WILL BE DONE
AND ONLY THE INPUT DATA PRINTED
- THE MAGNITUDE DATA WILL BE READ IN FASTER IF ARRANGED IN STATION ORDER
- 5) END OF JOB CARD FOR NORMAL END OF JOB
NORMAL END OF JOB WILL ALSO OCCUR IF NO MORE DATA
- REPEAT 1) TO 4) FOR ANY NUMBER OF MATRICES

THE INFORMATION IS PRINTED AS FOLLOWS --

TABLE 1 SETUP DATA
TABLE 1.1 STATIONS (UP TO 5 PAGES)
TABLE 1.2 EVENTS (UP TO 2 PAGES)

TABLE 2 INPUT MATRIX WITH WEIGHTS
PRINTS ALL STATIONS WITH EVENTS IN SETS OF 10 (UP TO 30 PAGES)

C
C TABLE 3 MATRIX OF RESIDUALS OF MAGNITUDES
C PRINTED AS TABLE 2 TRUE RESIDUALS ARE STARRED (UP TO 30 PAGES)
C
C TABLE 4 ANSWERS
C TABLE 4.1 STATION CORRECTIONS WITH 95 PERCENT CONFIDENCE LIMITS
C PRINTS OUT COMPUTED VALUES, STARS SMALLEST VALUE,
C NUMBER IN EACH ROW OF RESIDUALS,
C 95 PERCENT CONFIDENCE LIMITS, AND VARIANCE (UP TO 5 PAGES)
C TABLE 4.2 BEST ESTIMATE OF MAGNITUDES WITH 95 PERCENT CONFIDENCE
C PRINT OUT COMPUTED VALUES, (LIMITS
C NUMBER IN EACH COLUMN OF RESIDUALS,
C 95 PERCENT CONFIDENCE LIMITS, AND VARIANCE (UP TO 2 PAGES)
C
C TABLE 5 TRIANGULAR MATRIX OF DIFFERENCES OF MAGNITUDES
C PRINTS OUT DIFFERENCES WITH 95 PERCENT CONFIDENCE LIMITS
C (UP TO 42 PAGES)
C
C TABLE 6 VARIABLES USED DURING THE COMPUTATION (1 PAGE)

C
C

C
C SUBROUTINE LSNF
COMMON DATE,HEAD(9),NUM(60),AWT(60),N,NR,DISK,
1 XMEAN,CLM,VARM,RSQD,RBAR,ISTAN,STAN
COMMON /MTRCES/ A(261,261),B(261), P(60,200)
COMMON /ARRAYS/ X(261),Y(60),NRS(200),NRB(60),D(261),
1 CLX(261),CLY(60),VARX(261),VARY(60)
COMMON /CODES/ STN(200),SNAME,NST, EVENT(60),ECODE,NBT
COMMON /STUDT/ ST(57),T,IDF,NDF
INTEGER DISK
C
C DATA END(BHEND M), BLANK(8H)
C
C READ HEADING CARD AND ANY COMMENTS
10 CALL SECCLK(TS)
CALL HEADER
C
C ZERO MATRICES
20 DO 40 J=1,261
DO 30 I=1,261
A(I,J)=0.
30 CONTINUE

40 B(J)=0.
CONTINUE
DO 60 J=1,200
DO 50 I=1,60
P(I,J)=1000.
50 CONTINUE
NRS(J)=0
60 CONTINUE
DO 70 I=1,60
NRB(I)=0
70 CONTINUE
C
C SETUP STATIONS AND EVENTS
CALL SETUP
N=NST+NBT
C
C FORM MATRICES
NR=0
NS=1
100 IND=1
READ 105, SNAME,ECODE,AMAG,VWT
105 FORMAT(1X,A5,A8,2X,F13.9,I1)
NR=NR+1
IF(NWT) 110,110,120
110 NWT=1
120 WT=NWT
IF(SNAME.EQ.STN(NS)) GO TO 210
IF(SNAME.EQ.STN(NS+1)) GO TO 200
IF(SNAME.EQ.END) GO TO 300
150 DO 160 J=1,NST
IF(SNAME.EQ.STN(J)) GO TO 180
160 CONTINUE
IF(SNAME.EQ.BLANK) GO TO 290
PRINT 175, SNAME
175 FORMAT(27H1** UNKNOWN STATION NAME - ,A8//)
GO TO 280
180 DO 190 I=1,NBT
IF(ECODE.EQ.EVENT(I)) GO TO 250
190 CONTINUE
GO TO 230
200 NS=NS+1
210 DO 220 NB=1,NBT
IF(ECODE.EQ.EVENT(NB)) GO TO 240
220 CONTINUE
230 IF(ECODE.EQ.BLANK) GO TO 290
PRINT 235, ECODE
235 FORMAT(25H1** UNKNOWN EVENT CODE - ,A8//)

```

240 GO TO 280
    J=NS
    I=NB
250 P(I,J)=AMAG
    NRB(I)=NRB(I)+1
    NRS(J)=NRS(J)+1
    I=I+NST
260 A(I,J)=WT
    B(J)=B(J)+AMAG*WT
    GO TO (270,100),IND
270 IND=2
    NB=I
    I=J
    J=NB
    GO TO 260
280 PRINT 285
285 FORMAT(24H THE INCORRECT CARD IS -)
    PRINT 105, SNAME, ECODE, AMAG, NWT
    RETURN
290 CALL INPUT
    PRINT 295
295 FORMAT(30H1** ONLY INPUT PRINT REQUESTED///12H NO SOLUTION)
    GO TO 10
C
300 NR=NR-1
    LS=NST+1
    DO 320 J=1,NST
    AD=0.
    DO 310 I=LS,N
    AD=AD+A(I,J)
310 CONTINUE
    A(J,J)=AD
    A(J,N+1)=AD
    A(N+1,J)=AD
320 CONTINUE
    DO 340 J=LS,N
    AD=0.
    DO 330 I=1,NST
    AD=AD+A(I,J)
330 CONTINUE
    A(J,J)=AD
    A(J,N+1)=AD
    A(N+1,J)=AD
340 CONTINUE
    AD=0.

    AMAG=0.
    DO 350 J=1,N
    AD=AD+A(J,J)
    AMAG=AMAG+B(J)
350 CONTINUE
    A(N+1,N+1)=AD/2.
    B(N+1)=AMAG/2.
    DO 370 J=1,NST
    DO 360 I=1,NST
    A(I,J)=A(I,J)+1.
360 CONTINUE
370 CONTINUE
    DO 390 J=LS,N
    DO 380 I=LS,N
    A(I,J)=A(I,J)+1.
380 CONTINUE
390 CONTINUE
C
    PRINT INPUT
C
    CALL INPUT
    SOLVE MATRIX
C
    N=N+1
    DO 420 J=1,N
    IF(A(J,J)-1.)420,410,420
410 PRINT 415, J
415 FORMAT(20H1** DIAGONAL ELEMENT,14,6H ZERO///12H NO SOLUTION)
    GO TO 10
420 CONTINUE
    WRITE (DISK) ((A(I,J),I=1,N),J=1,N)
    CALL SOLVE(B,X,N,D)
    WRITE (DISK) ((A(I,J),I=1,N),J=1,N)
    REWIND DISK
    READ (DISK) ((A(I,J),I=1,N),J=1,N)
C
    SETUP STATION AND EVENT ARRAYS
    XMEAN=X(N)
    DO 470 I=1,NBT
    J=I+NST
    Y(I)=X(J)
470 CONTINUE
    STAN=ABS(X(I))
    ISTAN=I
    DO 490 J=2,NST
    IF(STAN-ABS(X(J)))490,490,480
480 STAN=ABS(X(J))
    ISTAN=J
490 CONTINUE

```

```

C                                     PRINT RESIDUALS
CALL OUTPUT
READ (DISK) ((A(I,J),I=1,N),J=1,N)
REWIND DISK

C                                     WORK OUT STUDENTS T
T=0.
NDF=NR-N+2
IF(NDF) 675,675,620
620 IF(NDF-30)630,640,640
630 IDF=NDF
GO TO 670
640 IF(NDF-300)650,660,660
650 IDF=NDF/10+27
GO TO 670
660 IDF=57
670 T=ST(IDF)

C                                     COMPUTE VARIANCES AND CONFIDENCE LIMITS
675 RBAR=0.
RSQD=0.
DO 690 J=1,NST
DO 680 I=1,NBT
AD=P(I,J)
RBAR=RBAR+AD
RSQD=RSQD+AD*AD
680 CONTINUE
690 CONTINUE
IF(NDF.GT.0) RSQD=RSQD/FLOAT(NDF)
DO 710 K=1,N
VARX(K)=RSQD/D(K)
CLX(K)=T*SQRT(VARX(K))
710 CONTINUE
DO 720 I=1,NBT
J=I+NST
VARY(I)=VARX(J)
CLY(I)=CLX(J)
720 CONTINUE
VARM=VARX(N)
CLM=CLX(N)
DO 740 I=1,NBT
J=I+NST
DO 730 LS=1,I
K=LS+NST
P(LS,I)=T*SQRT(RSQD*(ABS(A(K,K)+A(J,J))-2.*A(K,J)))
730 CONTINUE
740 CONTINUE

IF(NDF.GT.0) RSQD=RSQD*FLOAT(NDF)

C                                     PRINT ANSWERS
CALL TABLE
CALL TRIANG
CALL SECCLK(TF)
TS=TF-TS
PRINT 885, HEAD,DATE
885 FORMAT(55H1TABLE 6  VARIABLES USED DURING COMPUTATION
1 9A8/113X,6HDATE ,A8////)
PRINT 886, NR,N,RSQD,RBAR,T,NDF,XMEAN,CLM,TS
886 FORMAT(
1 33H          NUMBER OF READINGS = , 16          //
2 33H          NUMBER OF UNKNOWNNS = , 16          ////
3 33H  SUM OF SQUARES OF RESIDUALS = , F10.6       //
4 33H          SUM OF RESIDUALS = , E10.4         ////
5 33H          STUDENTS T = , F6.2              //
6 33H  NUMBER OF DEGREES OF FREEDOM = , 16         ////
7 33H  MEAN STATION-EVENT EFFECT = , F7.3,5H +/-,F7.5  //////////
8 33H  TIME TAKEN TO SOLVE MATRIX = , F7.3, 8H SECONDS)

C
C                                     LOOP FOR NEW MATRIX
GO TO 10
END

T      SUBTYPE,FORTAN,LMAP,LSTRAP
C      LSMF HEADING PRINT ROUTINE
C      *****
C
C      THIS ROUTINE READS AND PRINTS HEADING CARDS TILL IT FINDS A ZERO IN COL.80
C      THE CONTENTS OF THE FIRST CARD IS STORED IN ARRAY HEAD N.B. COLS.1-72 ONLY
C
SUBROUTINE HEADER
COMMON          DATE,HEAD(9)
DATA  END1(8H          EN),END2(8HD JOB  )

C
READ 1, HEAD,IT
FORMAT(9A8,7X,I1)
1 IF(HEAD(1).EQ.END1.AND.HEAD(2).EQ.END2) CALL EXIT
PRINT 2, DATE,HEAD
2 FORMAT(1H1/113X,6HDATE ,A8////25X,9A8////)
10 IF(IT) 20,30,20
20 READ 3, IT
PRINT 3
3 FORMAT(79H-----
1-----,I1)
GO TO 10

```

```

30 RETURN
END
T   SUBTYPE,FORTRAN,LMAP,LSTRAP
C   LSMF SETUP ROUTINE
C   *****
C   THIS ROUTINE SETS UP AND PRINTS STATIONS AND EVENTS
C
SUBROUTINE SETUP
COMMON DATE,HEAD(9)
COMMON /CODES/ STN(200),SNAME,NST, EVENT(60),ECODE,NBT
DATA END1(8HEND S ), END2(8HEND EVEN)
C
C                                     SETUP STATIONS
20 NST=0
   LINE=40
21 READ 22, SNAME
22 FORMAT(1X,A5,74H-----)
   IF(SNAME-END1)23,30,23
23 NST=NST+1
   IF(NST-200)26,24,24
24 PRINT 25
25 FORMAT(21H1** TOO MANY STATIONS)
   GO TO 41
26 IF(LINE-40)29,27,27
27 LINE=0
   PRINT 28, HEAD,DATE
28 FORMAT(55HITABLE 1.1 STATIONS
1  9A8/113X,6HDATE ,A8/
2  80H CODE STATION REGION LATITUDE LONGITUDE
3  CORRECTIONS /)
29 PRINT 22, SNAME
   LINE=LINE+1
   STN(NST)=SNAME
   GO TO 21
C
C                                     SETUP EVENTS
30 NBT=0
   LINE=40
31 READ 32, ECODE
32 FORMAT(6X,A8,66H-----)
   IF(ECODE-END2)33,40,33
33 NBT=NBT+1
   IF(NBT-60)36,34,34
C
34 PRINT 35
35 FORMAT(19H1** TOO MANY EVENTS)
   GO TO 41
36 IF(LINE-40)39,37,37
37 LINE=0
   PRINT 38, HEAD,DATE
38 FORMAT(55HITABLE 1.2 EVENTS
1  9A8/113X,6HDATE ,A8/
2  80H CODE EVENT DATA AND COMMENTS
3  /)
39 PRINT 32, ECODE
   LINE=LINE+1
   EVENT(NBT)=ECODE
   GO TO 31
C
C                                     FINISH FOR ERROR
40 RETURN
C
41 CALL EXIT
END
T   SUBTYPE,FORTRAN,LMAP,LSTRAP
C   LSMF INPUT PRINT ROUTINE
C   *****
C   THIS SUBROUTINE PRINTS OUT THE MATRIX OF MAGNITUDES (P)
C   WITH 1) ALL STATIONS
C   2) EVENTS IN SETS OF TEN (10)
C
C   PRINTS THE WEIGHT BY EACH MAGNITUDE READ IN
C   ZERO AND BLANK INDICATE NO VALUE
C
SUBROUTINE INPUT
COMMON DATE,HEAD(9),NUM(60),AWT(60)
COMMON /MTPCES/ A(261,261),B(261), P(60,200)
COMMON /CODES/ STN(200),SNAME,NST, EVENT(60),ECODE,NBT
DIMENSION FCHAR(10)
C
DATA (FCHAR(I),I=1,10) (80H *1 *2 *3 *4
1 *5 *6 *7 *8 *9 ), ANUM(8HEVENT )
C
J=0
420 J=J+10
   NB=J-9
   IF(J-NBT)440,440,430
430 J=NBT
440 LINE=40

```

```

DO 480 NS=1,NST
IF(LINE-40)460,450,450
450 LINE=0
PRINT 454, HEAD,DATE,(ANUM,NUM(I),I=NB,J)
454 FORMAT(5SHITABLE 2 MATRIX OF MAGNITUDES WITH WEIGHTS
1 9A8/113X,6HDATE ,AB/
2 9H STATION,4X,A5,13,9(4X,A5,13))
PRINT 455, (EVENT(I),I=NB,J)
455 FORMAT(13X,AB,9(4X,AB))
460 DO 470 I=NB,J
INST=I+NST
WT=A(INST,NS)
INST=[FIX(WT+0.5)+1
AWT(I)=FCHAR(INST)
470 CONTINUE
PRINT 475, NS,STN(NS),(P(I,NS),AWT(I),I=NB,J)
475 FORMAT(1X,13,2X,A6,F6.3,A3,9(3X,F6.3,A3))
LINE=LINE+1
480 CONTINUE
IF(J.NE.NBT) GO TO 420
RETURN
END

```

```

T SUBTYPE,FORTRAN,LMAP,LSTRAP
C LSMF MATRIX INVERSION ROUTINE
C *****

```

```

C THE METHOD USED IS CALLED TRIANGULAR DECOMPOSITION
C FROM N.P.L. MODERN COMPUTING METHODS

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C BASED ON LIBRARY SUBROUTINE MBO1A

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C SUBROUTINE SOLVE(B,X,M,D)
COMMON /MTRCES/ A(261,261)
COMMON /ARRAYS/ QQQ(902),C(261),IND(261)
DIMENSION B(M),X(M),D(M)

```

100	AMAX=0.0	MB01A003
	DO 2 I=1,M	MB01A004
	IND(I)=I	MB01A005
	IF(ABS(A(I,1))-AMAX)2,2,3	MB01A006
3	AMAX=ABS(A(I,1))	MB01A007
	I4=I	MB01A008
2	CONTINUE	MB01A009
	MM=M-1	MB01A010
	DO 111 J=1,MM	MB01A011
	IF(I4-J)6,6,4	MB01A012
4	ISTO=IND(J)	MB01A013
	IND(J)=IND(I4)	MB01A014
	IND(I4)=ISTO	MB01A015
	DO 5 K=1,M	MB01A016
	STO=A(I4,K)	MB01A017
	A(I4,K)=A(J,K)	MB01A018
	A(J,K)=STO	MB01A019
5	CONTINUE	MB01A020
6	AMAX=0.0	MB01A021
	J1=J+1	MB01A022
	DO 11 I=J1,M	MB01A023
	A(I,J)=A(I,J)/A(J,J)	MB01A024
	DO 10 K=J1,M	MB01A025
	A(I,K)=A(I,K)-A(I,J)*A(J,K)	MB01A026
	IF(K-J1)14,14,10	MB01A027
14	IF(ABS(A(I,K))-AMAX)10,10,17	MB01A028
17	AMAX=ABS(A(I,K))	MB01A029
	I4=I	MB01A030
10	CONTINUE	MB01A031
11	CONTINUE	MB01A032
111	CONTINUE	MB01A033
65	DO 140 I1=1,MM	MB01A034
	I=M+1-I1	MB01A035
	I2=I-1	MB01A036
	DO 41 J1=1,I2	MB01A037
	J=I2+1-J1	MB01A038
	J2=J+1	MB01A039
	W1=-A(I,J)	MB01A040
	IF(I2-J2)141,43,43	MB01A041
43	DO 42 K=J2,I2	MB01A042
	W1=W1-A(K,J)+C(K)	MB01A043
42	CONTINUE	MB01A044
141	C(J)=W1	MB01A045
41	CONTINUE	MB01A046
	DO 40 K=1,I2	MB01A047
	A(I,K)=C(K)	MB01A048
40	CONTINUE	MB01A049
140	CONTINUE	MB01A050
	DO 150 I1=1,M	MB01A051
	I=M+1-I1	MB01A052
	I2=I+1	MB01A053
	W=A(I,I)	MB01A054
	DO 56 J=1,M	MB01A055
	IF(I-J)52,53,54	MB01A056

```

52 W1=0.0
GO TO 55
53 W1=1.0
GO TO 55
54 W1=A(I,J)
55 IF(I-1)156,156,57
57 DO 58 K=1,M
W1=W1-A(I,K)*A(K,J)
58 CONTINUE
156 C(J)=W1
56 CONTINUE
DO 50 J=1,M
A(I,J)=C(J)/W
50 CONTINUE
150 CONTINUE
DO 60 I=1,M
63 IF(IND(I)-1)61,60,61
61 J=IND(I)
DO 62 K=1,M
STO=A(K,I)
A(K,I)=A(K,J)
A(K,J)=STO
62 CONTINUE
ISTO=IND(J)
IND(J)=J
IND(I)=ISTO
GO TO 63
60 CONTINUE
C
64 DO 66 J=1,M
STO=0.
DO 67 I=1,M
STO=STO+A(I,J)*B(I)
67 CONTINUE
X(J)=STO
D(J)=A(J,J)
66 CONTINUE
68 RETURN
END
T SUBTYPE,FORTRAN,LMAP,LSTRAP
C LSMF OUTPUT PRINT ROUTINE
C *****
C THIS ROUTINE COMPUTES AND PRINTS OUT THE MATRIX OF RESIDUALS OF MAGNITUDES P
C WITH 1) ALL STATIONS

C 2) EVENTS IN SETS OF TEN (10)
C
C N.B. THE TRUE RESIDUALS ARE PRINTED OUT
C BUT WEIGHTED RESIDUALS ARE RETURNED TO LSMF
C
C SUBROUTINE OUTPUT
COMMON DATE,HEAD(9),NUM(60),AWT(60),N,NR,DISK,
1 XMEAN,CLM,VARM,RSQD,RBAR,ISTAN,STAN
COMMON /MTRCES/ A(261,261),B(261), P(60,200)
COMMON /ARRAYS/ X(261),Y(60)
COMMON /CODES/ STN(200),SNAME,NST, EVENT(60),ECODE,NBT
INTEGER DISK
C
C DATA ANUM(8)EVENT ), STAR(8)* ), BLANK(8H )
C
J=0
420 J=J+10
NB=J-9
IF(J-NBT)440,440,430
430 J=NBT
440 LINE=40
DO 490 NS=1,NST
IF(LINE-40)460,450,450
450 LINE=0
PRINT 454, HEAD,DATE,(ANUM,NUM(I),I=NB,J)
454 FORMAT(55H1TABLE 3 MATRIX OF RESIDUALS OF MAGNITUDES
1 9A8/113X,6HDATE ,A8/
2 9H STATION,4X,A5,13,9(4X,A5,13))
PRINT 455, (EVENT(I),I=NB,J)
455 FORMAT(13X,A8,9(4X,A8))
460 DO 470 I=NB,J
IF(P(I,NS)-1000.)464,462,464
462 AWT(I)=BLANK
P(I,NS)=0.
GO TO 470
464 AWT(I)=STAR
P(I,NS)=P(I,NS)-X(NS)-Y(I)-XMEAN
470 CONTINUE
PRINT 475, NS,STN(NS),(P(I,NS),AWT(I),I=NB,J)
475 FORMAT(1X,13,2X,A6,F8.5,A1,9(3X,F8.5,A1))
LINE=LINE+1
DO 480 I=NB,J
INST=I+NST
P(I,NS)=P(I,NS)* A(INST,NS)
480 CONTINUE

```

```

MB01A057
MB01A058
MB01A059
MB01A060
MB01A061
MB01A062
MB01A063
MB01A064
MB01A065
MB01A066
MB01A067
MB01A068
MB01A069
MB01A070
MB01A071
MB01A072
MB01A073
MB01A074
MB01A075
MB01A076
MB01A077
MB01A078
MB01A079
MB01A080
MB01A081
MB01A082
MB01A083
MB01A084

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```

490 CONTINUE
   IF(J.NE.NBT) GO TO 420
   RETURN
   END
T   SUBTYPE,FORTRAN,LMAP,LSTRAP
C   LSMF TABLE PRINT SUBROUTINE
C   *****
C   THIS SUBROUTINE PRINTS OUT TABLES OF STATION AND EVENT CORRECTIONS
C
C   THE NUMBER, 95 PERCENT CONFIDENCE LIMITS, AND VARIANCE
C   ARE PRINTED OUT FOR EACH NUMBER
C
SUBROUTINE TABLE
COMMON DATE,HEAD(9),NUM(60),AWT(60),N,NR,DISK,
1 XMEAN,CLM,VARM,RSQD,RBAR,ISTAN,STAN
COMMON /MTRCES/ A(261,261),B(261), P(60,200)
COMMON /ARRAYS/ X(261),Y(60),NRS(200),NRB(60),D(261),
1 CLX(261),CLY(60),VARX(261),VARY(60)
COMMON /CODES/ STN(200),SNAME,NST, EVENT(60),ECODE,NBT
COMMON /STUDT/ ST(57),T,IOF,NDF
INTEGER DISK

DATA STAR(8H *** ), BLANK(8H )

C   PRINT OUT STATION CORRECTION
C
LINE=40
DO 350 NS=1,NST
IF(LINE=40)320,310,310
310 LINE=0
PRINT 315, HEAD,DATE
315 FORMAT(55HITABLE 4.1 STATION CORRECTIONS
1 9A8/113X,6HDATE ,A8/
2 119H STATION COMPUTED NUMBER 95 PERCENT
3 VARIANCE /
4 119H VALUE IN ROW CONFIDENCE LIMITS
5 )
320 IF(NS=ISTAN)330,325,330
325 DIAG=STAR
GO TO 340
330 DIAG=BLANK
340 PRINT 345, NS,STN(NS),X(NS),DIAG,NRS(NS),CLX(NS),VARX(NS)
345 FORMAT(1X,13,2X,A5,6X,F6.3,A6,15,6X,3H+/-,F8.5,6X,F8.6)
LINE=LINE+1
350 CONTINUE

C   PRINT OUT EVENT CORRECTION
C
LINE=40
DO 380 NB=1,NBT
IF(LINE=40)370,360,360
360 LINE=0
PRINT 365, HEAD,DATE
365 FORMAT(55HITABLE 4.2 BEST ESTIMATE OF MAGNITUDES
1 9A8/113X,6HDATE ,A8/
2 119H EVENT COMPUTED NUMBER 95 PERCENT
3 VARIANCE /
4 119H VALUE IN COL. CONFIDENCE LIMITS
5 )
370 PRINT 375, NB,EVENT(NB),Y(NB),NRB(NB),CLY(NB),VARY(NB)
375 FORMAT(1X,12,2X,A8,4X,F6.3,6X,15,6X,3H+/-,F8.5,6X,F8.6)
LINE=LINE+1
380 CONTINUE

C   RETURN
C   END
T   SUBTYPE,FORTRAN,LMAP,LSTRAP
C   LSMF TRIANGULAR MATRIX PRINT ROUTINE
C   *****
C   PRINTS THE LOWER TRIANGULAR MATRIX (P) IN SETS OF 5 EVENTS
C   FOR ALL EVENTS FROM THE START OF THE SET
C
SUBROUTINE TRIANG
COMMON DATE,HEAD(9),NUM(60),AWT(60)
COMMON /MTRCES/ A(261,261),B(261), P(60,200)
COMMON /ARRAYS/ X(261),Y(60)
COMMON /CODES/ STN(200),SNAME,NST, EVENT(60),ECODE,NBT
DATA ANUM(8HEVENT )

C
J=0
420 J=J+5
NB=J-4
IF(J=NBT)440,440,430
430 J=NBT
440 LINE=40
DO 450 NA=NB,NBT
IF(LINE=40)460,450,450
450 LINE=0
PRINT 454, HEAD,DATE,(ANUM,NUM(1),I=NB,J)
454 FORMAT(55HITABLE 5 MATRIX OF DIFFERENCES OF MAGNITUDES
1 9A8/113X,6HDATE ,A8/

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2 9H EVENT ,8X,A5,I3,4(15X,A5,I3)
PRINT 455, (EVENT(I),I=NR,J)
455 FORMAT(17X,A8,4(15X,A8))
460 DO 470 I=NR,J
    AWT(I)=Y(NA)-Y(I)
470 CONTINUE
    IF(NA-J)482,482,484
482 NC=NA
484 PRINT 485, NA,EVENT(NA),(AWT(I),P(I,NA),I=NR,NC)
485 FORMAT(1X,[2,2X,A8,5(F11.5,5H +/-,F7.5)]
    LINE=LINE+1
490 CONTINUE
    IF(J.NE.NBT) GO TO 420
RETURN
END

```

```

T SUBTYPE,DATA
12.70 4.30 3.18 2.78 2.57 2.45 2.36 2.31 2.26 2.23 2.20 2.18 2.16 2.14 2.13
2.12 2.11 2.10 2.09 2.09 2.08 2.07 2.07 2.06 2.06 2.06 2.05 2.05 2.05 2.04
2.02 2.01 2.00 2.00 1.99 1.99 1.99 1.98 1.98 1.98 1.98 1.98 1.98 1.97 1.97
1.97 1.97 1.97 1.97 1.97 1.97 1.97 1.97 1.96 1.96 1.96 1.96

```

```

START JOB
RUSSIAN LOG AMPLITUDE A/T KI ONLY 12/01/66 WSSS
STU STUTTGART* GERMANY 48 46 15.0N 9 16 36.0E
BOZ BOZEMAN* MONTANA 45 36 00.0N 111 38 00.0W
SCP STATE COLLEGE* PENNSYLVANIA 40 48 35.5N 77 52 09.8W
PRE PRETORIA* SOUTH AFRICA 25 45 00.0S 28 15 00.0E
NUR NURMIJARVI* FINLAND 60 30 32.4N 24 39 05.1E
NAI NAIROBI* KENYA 1 16 26.2S 36 48 13.2E
MAN MANILA* PHILIPPINES 14 40 00.0N 121 05 00.0E
KON KONCSBERG* NORWAY 59 38 57.0N 9 37 55.0E
KEV KEVO* FINLAND 69 45 21.2N 27 00 45.1E
IST ISTANBUL* TURKEY 41 02 36.0N 28 59 06.0E
GOL GOLDEN* COLORADO 39 42 01.0N 105 22 16.0W
GEO GEORGETOWN* WASHINGTON DC 38 54 00.0N 77 04 00.0W
FLO FLORISSANT* MISSOURI 38 48 06.0N 90 22 12.0W
DAL DALLAS* TEXAS 32 50 46.0N 96 47 02.0W
COL COLLEGE OUTPOST ALASKA 64 54 00.0N 147 47 36.0W
BUL BULAWAYO* RHODESIA 20 08 36.0S 28 36 48.0E
ALQ ALBUQUERQUE* NEW MEXICO 34 56 30.0N 106 27 30.0W
SHI SHIRAZ* IRAN 29 38 40.2N 52 31 34.1E
AAM ANN ARBOR* MICHIGAN 42 17 59.0N 83 39 22.0W
MUN MUNDARING* AUSTRALIA 31 58 30.0S 116 12 24.0E
BAG BAGUIO CITY* PHILIPPINES 16 24 39.0N 120 34 47.0E
NDR NORC* GREENLAND 81 36 00.0N 16 41 00.0W
ATL ATLANTA* GEORGIA 33 26 00.0N 84 20 15.0W

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MAL MALAGA* SPAIN 36 43 39.0N 4 24 40.0W
TOL TOLEDO* SPAIN 39 52 53.0N 4 02 55.0W
ESK ESKDALEMUIR* SCOTLAND 55 19 00.0N 3 12 18.0W
TRI TRIESTE* ITALY 45 42 32.0N 13 45 51.0E
COP COPENHAGEN* DENMARK 55 41 00.0N 12 26 00.0E
BLA BLACKSBURG* VIRGINIA 37 12 40.0N 80 25 14.0W
ATU ATHENS UNIV.* GREECE 37 58 22.0N 23 43 00.0E
AKU AKUREYRI* ICELAND 65 41 12.0N 18 06 24.0W
KOD KODAIKANAL* INDIA 10 14 00.0N 77 28 00.0E
LON LONGMIRE* WASHINGTON 46 45 00.0N 121 48 36.0W
NDI NEW DELHI* INDIA 28 41 00.0N 77 13 00.0E
POO POONA* INDIA 18 32 00.0N 73 51 00.0E
SEO SEOUL* KOREA 37 34 00.0N 126 58 00.0E
WIN WINDHOEK* SOUTH AFRICA 22 34 00.0S 17 06 00.0E
COR CORVALLIS* OREGON 44 35 08.6N 123 18 11.5W
PEL PELCEHUE* CHILE 33 08 37.0S 70 41 07.0W
ANT ANTOFAGASTA* CHILE 23 42 18.0S 70 24 55.0W
ARE AREQUIPA* PERU 16 27 43.5S 71 29 28.6W
LPB LA PAZ* BOLIVIA 16 31 57.6S 68 05 54.1W
RCD RAPID CITY* SOUTH DAKOTA 44 04 30.0N 103 12 30.0W
TAU TASMANIA UNIV.* TASMANIA 42 54 35.7S 147 19 13.5E
MNN MINNEAPOLIS* MINNESOTA 44 54 52.0N 93 11 24.0W
PMG PORT MORESBY* NEW GUINEA 9 24 33.0S 147 09 14.0E
AQU AQUILA* ITALY 42 21 14.0N 13 24 11.0E
BKS BYERLY* CALIFORNIA 37 52 36.0N 122 14 06.0W
GDH GODHAVN* GREENLAND 69 15 00.0N 53 32 00.0W
CHG CHIENGMAI* THAILAND 18 47 24.0N 98 58 37.0E
CTA CHARTERS TOWERS* AUSTRALIA 20 05 18.0S 146 15 16.0E
QUE QUETTA* PAKISTAN 30 11 18.0N 66 57 00.0E
KTG KAP TOBIN* GREENLAND 70 25 00.0N 21 59 00.0W

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```

END STATIONS
R1150364
R1160564
R1190764
R1161164
R1040265
R1030365
R1110565
END EVENTS

```

```

STU R1030365 2.20
STU R1150364 2.30
STU R1160564 2.20
STU R1190764 2.00
STU R1161164 2.30
STU R1040265 2.21

```

BOZ	R1030365	1.58
BOZ	R1150364	1.70
BOZ	R1160564	1.70
BOZ	R1190764	1.50
BOZ	R1161164	1.76
BOZ	R1110565	0.78
SCP	R1150364	1.30
SCP	R1161164	1.60
PRE	R1030365	1.19
PRE	R1150364	1.08
PRE	R1160564	1.00
PRE	R1190764	0.80
PRE	R1161164	1.11
NUR	R1150364	1.60
NUR	R1160564	1.70
NUR	R1190764	1.50
NAI	R1030365	1.58
NAI	R1150364	1.30
NAI	R1160564	1.40
NAI	R1040265	1.30
MAN	R1030365	2.09
MAN	R1150364	2.20
MAN	R1190764	2.00
MAN	R1161164	2.20
MAN	R1040265	2.20
KON	R1030365	1.67
KON	R1160564	1.90
KON	R1110565	1.00
KEV	R1150364	1.70
KEV	R1160564	1.60
IST	R1030365	1.62
IST	R1150364	1.80
IST	R1160564	1.70
IST	R1190764	1.70
IST	R1161164	1.84
GOL	R1030365	1.18
GOL	R1150364	1.08
GOL	R1160564	1.08
GOL	R1190764	0.90
GOL	R1161164	1.36
GEO	R1150364	1.20
GEO	R1160564	1.30
FLO	R1150364	1.08
FLO	R1160564	1.08
FLO	R1161164	1.23

DAL	R1150364	1.08
DAL	R1161164	1.41
COL	R1030365	1.85
COL	R1150364	1.90
COL	R1160564	2.00
COL	R1190764	1.80
COL	R1161164	1.97
COL	R1110565	1.18
BUL	R1030365	1.30
BUL	R1150364	1.50
BUL	R1160564	1.50
BUL	R1190764	1.40
BUL	R1161164	1.37
BUL	R1040265	1.48
ALQ	R1030365	0.70
ALQ	R1150364	0.90
ALQ	R1160564	0.90
ALQ	R1190764	0.80
SHI	R1030365	1.81
SHI	R1160564	1.90
SHI	R1190764	1.80
SHI	R1161164	1.91
SHI	R1110565	0.81
AAM	R1030365	1.30
AAM	R1160564	1.50
AAM	R1190764	1.56
AAM	R1161164	1.55
MUN	R1160564	1.50
MUN	R1190764	1.40
MUN	R1161164	1.53
BAG	R1150364	1.77
BAG	R1160564	1.80
BAG	R1190764	1.60
NOR	R1190764	1.73
NOR	R1161164	1.73
ATL	R1160564	1.08
ATL	R1161164	1.15
MAL	R1160564	1.80
MAL	R1190764	1.60
MAL	R1161164	1.74
TOL	R1160564	2.09
TOL	R1190764	1.90
TOL	R1161164	2.00
ESK	R1030365	1.83
ESK	R1160564	2.00

ESK	R1161164	1.91
ESK	R1110565	0.90
TRI	R1160564	1.80
TRI	R1190764	1.70
COP	R1190764	1.70
COP	R1040265	2.06
BLA	R1161164	1.18
ATU	R1040265	1.90
ATU	R1161164	1.78
AKU	R1030365	1.90
AKU	R1161164	1.95
KOD	R1030365	1.82
KOD	R1161164	1.94
LON	R1030365	1.53
LON	R1161164	1.65
LON	R1110565	0.81
NDI	R1110565	1.84
NDI	R1030365	2.71
POO	R1030365	1.60
POO	R1161164	1.60
POO	R1040265	1.70
SEO	R1161164	1.34
WIN	R1161164	1.30
COR	R1161164	1.95
PEL	R1161164	1.40
ANT	R1040265	1.52
ANT	R1030365	1.48
ARE	R1030365	0.96
LPB	R1161164	0.60
RCD	R1030365	1.30
TAU	R1161164	1.30
MNN	R1161164	2.11
PMG	R1040265	1.82
PMG	R1030365	1.60
PMC	R1150364	1.68
PMG	R1161164	1.78
AQU	R1161164	1.48
BKS	R1161164	1.55
GDH	R1040265	1.72
CHG	R1030365	1.70
CTA	R1030365	1.23
QUE	R1030365	2.06
KTC	R1030365	1.56
END	MAGNITUDES	
	END JOB	

